### Role of the surface state of Ni/Al<sub>2</sub>O<sub>3</sub> in partial oxidation of CH<sub>4</sub>

Chunyi Li a,\*, Changchun Yu b and Shikong Shen b

<sup>a</sup> Department of Chemical Engineering, University of Petroleum, Dongying, Shandong Province 257062, PR China
 E-mail: chyli@sunctr.hdpu.edu.cn

<sup>b</sup> Catalytic Key Laboratory of CNPC, University of Petroleum, Changping, Beijing 102200, PR China

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The effect of gas phase  $O_2$  and reversibly adsorbed oxygen on the decomposition of  $CH_4$  and the surface state of a Ni/Al<sub>2</sub>O<sub>3</sub> catalyst during partial oxidation of  $CH_4$  were studied using the transient response technique at atmospheric pressure and  $700\,^{\circ}C$ . The results show that, when the catalyst surface is completely oxidized under experimental conditions, only a small amount of CO and CO

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#### 1. Introduction

The study on the conversion of natural gas containing mostly CH<sub>4</sub> to value-added products, such as easily transportable fuels, via direct or indirect methods is driven by the tremendous abundance of natural gas [1]. Direct conversion of CH<sub>4</sub>, for example oxidative coupling of CH<sub>4</sub>, has met some difficulty. Indirect conversion of CH<sub>4</sub> via syngas is promising, so economical production of syngas from CH<sub>4</sub> has been a hotspot of research.

Partial oxidation of CH<sub>4</sub> to syngas has the following advantages over the conventional steam reforming process: (i) the syngas with low H<sub>2</sub>/CO ratio ( $\sim$ 2) is suitable for methanol and Fischer–Tropsch synthesis; (ii) partial oxidation of CH<sub>4</sub> is a slightly exothermic reaction and is much more energy-efficient than steam reorming of CH<sub>4</sub> which is highly endothermic; (iii) a smaller reactor can be used to achieve high CH<sub>4</sub> conversion and selectivities to CO and H<sub>2</sub> with short contact time ( $\leq$ 10<sup>-2</sup> s); and (iv) partial oxidation of CH<sub>4</sub> is mechanically simpler than the steam reforming process, since it is completed within a single train, and does not need any external heaters [2–4]. Consequently, partial oxidation of CH<sub>4</sub> to syngas has attracted even more attention of researchers in recent years.

The reaction mechanism of partial oxidation of  $CH_4$  has evoked controversies. Some authors [5–8] pointed out that the partial oxidation of  $CH_4$  to syngas proceeds via an indirect oxidation mechanism, namely: complete combustion of  $CH_4$  to  $CO_2$  and  $H_2O$  and a subsequent reforming reac-

tion of the residual  $CH_4$  with  $CO_2$  and  $H_2O$  to CO and  $H_2$ . However, other authors [9–11] claimed that CO and  $H_2$  are produced directly while  $CO_2$  is formed by further oxidation of CO. Besides, parallel formation of CO and  $CO_2$  has also been suggested over transition metals supported on metal oxide [12]. Tang et al. [2] investigated the reaction mechanism over  $Pt/Al_2O_3$  using the deuterium isotope effect with the pulse MS method and their experimental results supported the parallel mechanism. Our work [13,14] on partial oxidation of  $CH_4$  to syngas over  $Ni/Al_2O_3$  supports the direct oxidation mechanism.  $CH_4$  decomposes on active metallic Ni sites to  $H_2$  and  $Ni_xC$ , and then  $Ni_xC$  reacts with NiO formed by oxidation of metallic Ni by  $O_2$  to CO or  $CO_2$  depending on the concentration of NiO around  $Ni_xC$ .

It should be mentioned that partial oxidation of CH<sub>4</sub> to syngas is a complicated process [2]. Different pre-treating conditions or different surface states of the catalyst may affect its reactivity and selectivity, and even may change the reaction mechanism. In this paper, the transient response technique has been used to investigate the effects of gas phase O<sub>2</sub>, reversibly adsorbed oxygen species, NiO on the Ni/Al<sub>2</sub>O<sub>3</sub> catalyst surface, and the surface state of the catalyst in partial oxidation of CH<sub>4</sub>. Some new evidences for the direct oxidation mechanism are given, and the reasons of high selectivity to CO are also discussed.

### 2. Experimental

The 8% (mol, Ni/(Ni + Al)) Ni/Al $_2$ O $_3$  catalyst was prepared by co-precipitation with a 1 mol/l mixture solution of

<sup>\*</sup> To whom correspondence should be addressed.

 $Ni(NO_3)_2$  and  $Al(NO_3)_3$  using a 1 mol/l  $NH_4OH$  solution as the precipitant. The pH of the solution was maintained at 7.5 during precipitation. The precipitate was aged for 6 h, filtered, washed with distilled water, dried at  $100\,^{\circ}C$  for 10 h, then calcined in air at  $400\,^{\circ}C$  for 10 h, crushed and sieved to 0.3–0.45 mm. The BET surface area and the dispersion of Ni on  $Al_2O_3$  measured by ASAP2010 are  $280\,$  m<sup>2</sup>/g and about 5%, respectively.

The experimental apparatus has been depicted elsewhere [13]. All experiments were carried out in a fixed-bed quartz microreactor 5.5 mm in diameter at atmospheric pressure and  $700\,^{\circ}\text{C}$ , and the total flow rate was 30 ml/min. 30 mg Ni/Al<sub>2</sub>O<sub>3</sub> catalyst was placed in the middle part of the reactor and the other space was filled with 0.45–0.9 mm quartz. The furnace was controlled by an AI-FUZZY temperature controller with linear heating rate between room temperature and  $850\,^{\circ}\text{C}$ . Heating rates between 1 and  $30\,^{\circ}\text{C/min}$  are possible. The temperature was measured by a K-type thermocouple.

Transient switch was operated with a four-way valve and pulse experiments were performed using a six-way sampling valve with a 0.39 ml quantifying tube. The effluents of the reactor were monitored by a quadrupole mass spectrometer (AMTEK QuadLink 1000) with the minimum dwell time of 3 ms.

XRD characterization of catalyst samples was conducted with BDX3200 X-ray powder diffractometer made by Qingniao Company of Beijing University.

#### 3. Results

3.1. Alternative pulses of  $O_2$  and CO with different time intervals and transient experiments from 1/1  $O_2/He$  to Ar

After three  $O_2$  pulses with 10 s intervals over the Ni/Al<sub>2</sub>O<sub>3</sub> catalyst pre-reduced at 700 °C for 1 h, a CO pulse was carried out with different time intervals between the third  $O_2$  pulse and the CO pulse. The results are shown in figure 1 (only the third  $O_2$  pulse was drawn). With the increase of the time interval between the  $O_2$  and CO pulses, the quantity of  $CO_2$  formed by the oxidation of CO pulsed after the  $O_2$  pulse decreases.

In 30 mg catalyst, there are about 46  $\mu$ mol Ni atoms and 2.3  $\mu$ mol on the catalyst surface. For each  $O_2$  pulse, there are about 32  $\mu$ mol oxygen atoms. Ni is very easy to be oxidized under the experimental conditions. Therefore, after three  $O_2$  pulses, nearly all the Ni atoms on the catalyst surface are oxidized to NiO. We have proved that CO is more difficult to be oxidized by NiO at 700 °C [15], so there must be other oxygen species on the catalyst surface with higher oxidative activity. We consider they are adsorbed oxygen species. To get more direct evidence, we did the transient experiments from 30 ml/min 1/1  $O_2$ /He to the same flow rate pure Ar with and without catalyst in the reactor, respectively. The results are shown in figure 2.

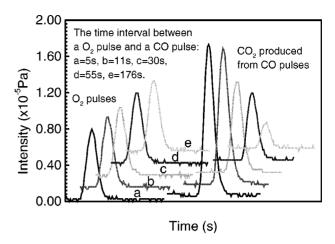


Figure 1. Alternative pulses of O2 and CO with different time intervals.

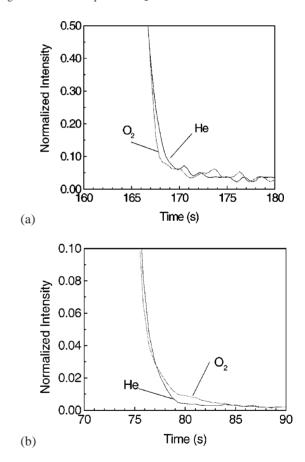


Figure 2. Responses of the transient from 30 ml/min 1/1  $O_2$ /He to 30 ml/min pure Ar at 700 °C. (a) Without catalyst in the reactor, (b) with 30 mg Ni/Al<sub>2</sub>O<sub>3</sub> in the reactor.

If  $O_2$  can be adsorbed on the catalyst at  $700\,^{\circ}$ C, as compared to the case without catalyst but with only quartz sand in the reactor, the  $O_2$  transient decreasing response would delay somewhat. In fact, with He tracer as the reference, the  $O_2$  transient decreasing response with catalyst in the reactor (figure 2(b)) has a little trailing as compared with that without catalyst (figure 2(a)). This illustrates that there must be a small quantity of reversibly adsorbed oxygen species that are in equilibrium with gas phase  $O_2$ . When the ambience

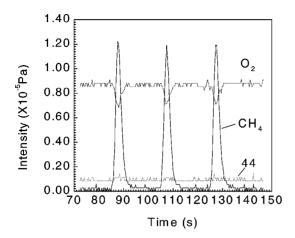


Figure 3. CH<sub>4</sub> pulses in 30 ml/min  $O_2$  at 700  $^{\circ}$ C without catalyst in the reactor.

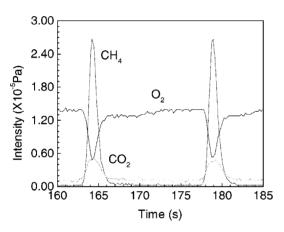


Figure 4. CH<sub>4</sub> pulses in O<sub>2</sub> atmosphere at 700 °C over the Ni/Al<sub>2</sub>O<sub>3</sub> catalyst.

is changed to  $O_2$ -free Ar gas, they desorb quickly and a slight trailing is left in the responses of  $O_2$ .

#### 3.2. $CH_4$ pulses in $O_2$ gas flow

Reversibly adsorbed oxygen is much more active than NiO in oxidizing CO at atmospheric pressure and  $700\,^{\circ}$ C [15]. Whether or not it is also active to oxidize CH<sub>4</sub> is our concern. Before investigation, we must know whether the gas phase reaction of CH<sub>4</sub> and O<sub>2</sub> may occur under the experimental conditions.

Without catalyst in the reactor,  $CH_4$  pulses were conducted in 30 ml/min  $O_2$  gas flow at atmospheric pressure and 700 °C, and no significant  $CO_2$  was detected (figure 3), which means that a gas phase oxidation reaction between  $CH_4$  and  $O_2$  does not occur under these conditions.

The above experiments were repeated with 30 mg Ni/Al $_2O_3$  catalyst in the reactor, and corresponding to each CH $_4$  pulse CO $_2$  appeared obviously, but no CO and H $_2$  were detected (figure 4). These results demonstrate the occurrence of a catalytic oxidation reaction. However, we cannot confirm that the CO $_2$  is from the reaction between CH $_4$  and adsorbed oxygen, for it is also possible that CH $_4$  reacts with NiO to form CO $_2$ .

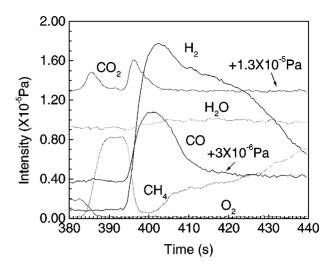


Figure 5. Responses of transient from 1/2 O<sub>2</sub>/He to 2/1 CH<sub>4</sub>/Ar over the catalyst oxidized for 1 h.

## 3.3. Transient experiments from 1/2(mol) O<sub>2</sub>/Ar to 2/1(mol) CH<sub>4</sub>/He

The catalyst was first oxidized in 30 ml/min 1/2 O<sub>2</sub>/Ar gas flow for 1 h at 700 °C, then a transient switch to the same flow rate 2/1 CH<sub>4</sub>/He was performed (figure 5). We can only detect a small amount of CO<sub>2</sub> just after the switch, and 3-4 s hereafter (389-393 s in figure 5) nearly no product is detected, then CH<sub>4</sub> starts to decompose. Accompanying the formation of H<sub>2</sub>, a great deal of CO and CO<sub>2</sub> are produced. This indicates that there are oxygen species on the catalyst surface before the CH<sub>4</sub> decomposition. According to the residence time of the reversibly adsorbed oxygen and the quantity of CO and CO<sub>2</sub> produced here, we can infer that the catalyst is still in the oxidative form, that is, most of Ni on the catalyst surface is in the form of NiO before CH<sub>4</sub> decomposition. Since nearly no product is formed between the first CO<sub>2</sub> peak and CH<sub>4</sub> decomposition (389-393 s in figure 5), the conclusions that CH<sub>4</sub> cannot be oxidized by NiO and that the first CO<sub>2</sub> peak is the product from CH<sub>4</sub> oxidized by reversibly adsorbed oxygen can be made.

# 3.4. Transient experiments from 2/1(mol) CH<sub>4</sub>/O<sub>2</sub> to 2/1(mol) CH<sub>4</sub>/He and from 2/1(mol) CH<sub>4</sub>/O<sub>2</sub> to pure He

The transient decreasing responses of CO and CO<sub>2</sub> from 2/1 CH<sub>4</sub>/O<sub>2</sub> to 2/1 CH<sub>4</sub>/He and from 2/1 CH<sub>4</sub>/O<sub>2</sub> to pure He after the reaction of 2/1 CH<sub>4</sub>/O<sub>2</sub> proceeding for 5 min at 700 °C over the catalyst pre-reduced for 1 h are shown in figure 6. The decreasing trends of CO and CO<sub>2</sub> in both cases are nearly the same, which indicates that there is no surplus oxygen on the catalyst surface. Otherwise CO and/or CO<sub>2</sub> will be produced continuously after the switch from 2/1 CH<sub>4</sub>/O<sub>2</sub> to 2/1 CH<sub>4</sub>/He and the decreasing responses will have some delay as compared to that from 2/1 CH<sub>4</sub>/O<sub>2</sub> to pure He. So the catalyst surface is maintained in the reduced state during partial oxidation of CH<sub>4</sub>, as has also been proved by XRD characterization for the catalyst sample over which partial oxidation of CH<sub>4</sub> proceeded for

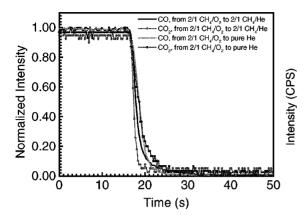


Figure 6. Decreasing responses of CO and CO $_2$  transient from 2/1 CH $_4$ /O $_2$  to 2/1 CH $_4$ /He and from 2/1 CH $_4$ /O $_2$  to pure He with total flow rate 30 ml/min over the Ni/Al $_2$ O $_3$  catalyst pre-reduced for 1 h and after partial oxidation of CH $_4$  proceeding for 5 min at atmospheric pressure and 700 °C.

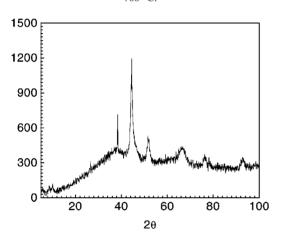


Figure 7. XRD characterization for the Ni/Al $_2$ O $_3$  catalyst over which partial oxidation of CH $_4$  has proceeded for 5 h at 700  $^{\circ}$ C.

5 h (figure 7). In the figure, three Ni peaks ( $2\theta = 44.6^{\circ}$ ,  $51.3^{\circ}$  and  $76.3^{\circ}$ ) were detected, and there were no NiO peaks. The result is consistent with those of the transient experiments.

# 3.5. Transient experiments from 2/1(mol) $CH_4/O_2$ to 2/1(mol) $He/O_2$

The transient switch from 2/1 CH<sub>4</sub>/O<sub>2</sub> to He/O<sub>2</sub> was performed after CH<sub>4</sub>/O<sub>2</sub> had reacted for 5 min over the catalyst pre-reduced at  $700\,^{\circ}$ C. The results are shown in figure 8. After the switch, the intensity of CO<sub>2</sub> first increased, and then decreased slowly to the base line, which denotes the formation of CO<sub>2</sub>. However, whether CO<sub>2</sub> comes from the oxidation of surface carbon species is not clear. To confirm this, we must exclude the possibility of the formation of CO<sub>2</sub> in the reaction between CH<sub>4</sub> and oxygen. Thus, the following experiments were performed: after the reaction of CH<sub>4</sub>/O<sub>2</sub> over the catalyst pre-reduced at  $700\,^{\circ}$ C proceeding for 5 min, the ambience was first switched to pure He to sweep the catalyst bed for 2 min, and then switched to 2/1 He/O<sub>2</sub>. The results are shown in figure 9, in which sig-

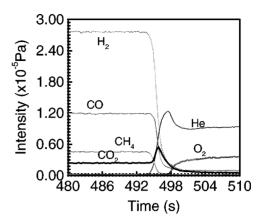


Figure 8. Transient responses from 2/1  $CH_4/O_2$  to 2/1  $He/O_2$  after partial oxidation of  $CH_4$  for 5 min.

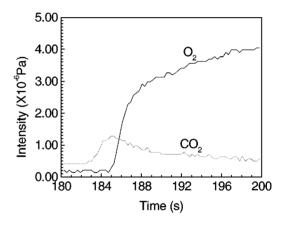


Figure 9. Reaction of 2/1 He/O<sub>2</sub> with the catalyst flushed by pure He for 2 min after partial oxidation of CH<sub>4</sub> for 5 min.

nificant  $CO_2$  production can be seen. Consequently, there must be a certain amount of carbon species on the catalyst surface.

# 3.6. Temperature-programmed reaction of 2/1(mol) $CH_4/O_2$ over the reduced catalyst

Temperature-programmed reaction of 2/1 CH<sub>4</sub>/O<sub>2</sub> at the rate of 26 °C/min was conducted after the Ni/Al<sub>2</sub>O<sub>3</sub> catalyst had been reduced for 1 h at 700 °C. The results are shown in figure 10.

 $CO_2$  and  $H_2O$  are produced originally at about 430 and at 600 °C CO and  $H_2$  appear. The intensities of these products increase with the increase of temperature and remain nearly unchanged when the temperature is maintained at 700 °C. Here, the conversions of  $CH_4$  and  $O_2$  are 7.92 and about 10%, and the selectivities to  $H_2$  and CO are 76.6 and 41.0%, respectively.

When the  $O_2$  mass flow controller is closed, the intensity of  $CH_4$  increases quickly, but all the intensities of  $H_2$ ,  $O_2$ , CO and  $CO_2$  decrease. About 40 s later,  $CH_4$  starts to decompose, and  $H_2$  and CO are produced at the same time. The results are similar to that in figure 5 and indicate that the surface of the catalyst is in the oxidative state during the temperature-programmed reaction. When the  $O_2$  mass flow

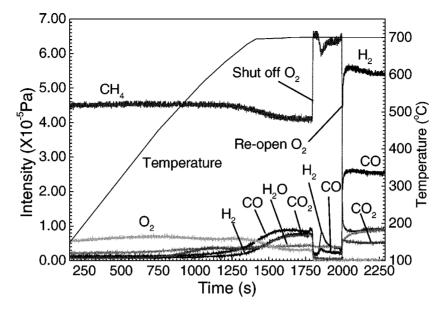


Figure 10. Temperature-programmed reaction of partial oxidation of methane conducted over a pre-reduced Ni/Al $_2$ O $_3$  catalyst with the rate of 26  $^{\circ}$ C/min. O $_2$  was shut off for a few minutes when the temperature reached 700  $^{\circ}$ C and then retrieved.

controller is turned on again, the conversion of  $CH_4$  and the selectivities to  $H_2$  and CO are improved significantly, which are 81.3, 87.7 and 82.4%, respectively, and  $O_2$  is consumed completely.

### 4. Discussion

### 4.1. The effect of different oxygen species on CH<sub>4</sub> adsorption and decomposition

Our previous work [13,14] has shown that Ni on the catalyst surface exists in the form of NiO after being oxidized for 1 h and there is a small amount of reversibly adsorbed oxygen on the catalyst. Reversibly adsorbed oxygen is more active than NiO in oxidizing CO [15]. In figures 4 and 5, it is evident that CH<sub>4</sub> is easy to be oxidized by adsorbed oxygen but difficult by NiO.

It can be seen from figure 4 that corresponds to each  $CH_4$  pulse, only  $CO_2$  is produced. In figure 5, after switching to  $CH_4$ , nevertheless, only  $CO_2$  appears immediately. And there is a certain time during which nearly no product is formed before  $CH_4$  starts to decompose. All these illustrate  $CH_4$  cannot decompose over NiO. Active metallic Ni sites are needed for  $CH_4$  decomposition [13,14].

Chen et al. [16] suggested that a certain amount of NiO in NiO crystal can dissociate without gas phase  $O_2$  at  $700\,^{\circ}$ C, so the atomic ratio of Ni/O is higher than the stoichiometric ratio. It is known that a single metal atom has no catalytic activity and a defective surface is more active [17]. Furthermore, when the environment changes, restructuring will occur on the surface of some metal crystals, such as Ir, Pt, Au, and semiconductors Si, Ge, GaAs, InSb, etc., and extends from the outer layer to several atom layers inside [18]. In our opinion, before CH<sub>4</sub> begins to decompose after the switch, zero-valence Ni atoms are formed on the oxidized catalyst surface, and these metallic Ni may

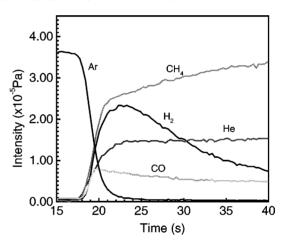


Figure 11. Responses of transient from pure Ar to 2/1 CH<sub>4</sub>/He over the catalyst oxidized in 30 ml/min 1/2  $O_2$ /Ar gas flow for 1 h and then swept with pure Ar for 3 min.

be rearranged. When such metallic Ni site needed for CH<sub>4</sub> decomposition is formed, CH<sub>4</sub> starts to decompose on these sites.

We define the time from the switch to the decomposition of  $CH_4$  the induction period, during which  $CH_4$  is first oxidized fully to  $CO_2$  and  $H_2O$  by reversibly adsorbed oxygen on the catalyst and then metallic Ni atoms are formed and rearranged to form active metallic Ni sites for  $CH_4$  decomposition.

To validate the above viewpoints, the catalyst was first swept with pure Ar for 3 min after being oxidized in 30 ml/min 1/2 O<sub>2</sub>/Ar gas flow for 1 h at 700 °C, then a transient switch was performed from Ar to 2/1 CH<sub>4</sub>/He. The results are shown in figure 11. After the switch, CH<sub>4</sub> almost decomposes immediately and no induction period appears. In fact, here the induction period has already finished during the sweep with pure Ar (figure 11).

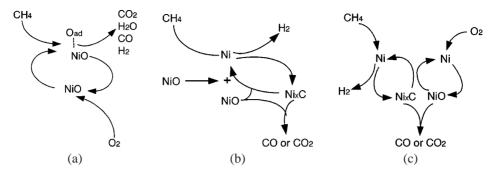


Figure 12. Schematic reaction mechanisms corresponding to figure 10: (a) before shutting off  $O_2$ , (b) after shutting off  $O_2$  and (c) for re-opened  $O_2$ .

In figure 5, the first  $CO_2$  peak is the result of the reaction between reversibly adsorbed oxygen and  $CH_4$  via the Rideal–Eley mechanism, and the second one is the result of surface reaction of NiO and  $Ni_xC$  formed by  $CH_4$  decomposition. The nature of these reactions is different. NiO cannot oxidize  $CH_4$  directly, and it has difficulty in oxidizing CO, therefore, the high selectivity of CO during partial oxidation of  $CH_4$  is closely related to these factors.

# 4.2. The surface state of $Ni/Al_2O_3$ catalyst during partial oxidation of $CH_4$

According to figure 6, once NiO is produced on the catalyst surface during partial oxidation of  $CH_4$ , it reacts immediately with  $Ni_xC$  from  $CH_4$  decomposition to form a large amount of CO and a small amount of  $CO_2$ . Moreover, a part of NiO can also react with hydrogen from  $CH_4$  decomposition to form  $H_2O$ . The catalyst surface maintains its reduced state. This is the precondition for partial oxidation of  $CH_4$ . If the catalyst surface has been oxidized before partial oxidation of  $CH_4$  begins, the reaction mechanism will change. This will be discussed below.

On the catalyst surface, there is a small amount of carbon species (figures 8 and 9), which is favorable for keeping the catalyst from being oxidized, and for improving the selectivity to CO because the existence of carbon species can restrain the production of  $CO_2$  to some extent.

### 4.3. The effect of surface state on the reaction mechanism

Slagtern et al. [19] found that the conversion of  $CH_4$  and the selectivities to CO and  $H_2$  over a Ni-based catalyst at increasing temperature are lower than that at decreasing temperature before the complete consumption of  $O_2$  at temperature below  $800\,^{\circ}C$ . These phenomena are similar to our results of temperature-programmed reaction shown in figure 10. The results predict that different surface states correspond to different reaction mechanisms.

Our previous work [13,14] has shown that partial oxidation of  $CH_4$  over a  $Ni/Al_2O_3$  catalyst proceeds via a direct oxidation mechanism, and  $CH_4$  decomposes first on the active metallic Ni sites to  $H_2$  and  $Ni_xC$ . However, in figure 8, after closing the  $O_2$  mass flow controller, the intensity of  $H_2$  decreases together with that of  $O_2$ , CO and  $CO_2$ , which implies that the  $H_2$  produced is not from  $CH_4$  decomposi-

tion over the active metallic Ni sites. Therefore, during the temperature-programmed reaction, the reaction is not via a direct oxidation mechanism.

According to the experimental results of temperatureprogrammed reaction, different mechanisms corresponding to different stages in figure 10 are suggested (figure 12).

During the temperature-programmed reaction, there is competitive adsorption between CH<sub>4</sub> and O<sub>2</sub> on metallic Ni sites, and O<sub>2</sub> adsorption is stronger than that of CH<sub>4</sub>. Therefore, metallic Ni sites have been oxidized before the temperature is raised high enough for CH<sub>4</sub> decomposition. CH<sub>4</sub> cannot decompose on oxidized Ni sites, and NiO cannot oxidize CH<sub>4</sub>. But CH<sub>4</sub> can be oxidized by reversibly adsorbed oxygen, which exists on the oxidized surface in the presence of O<sub>2</sub> in the system, via the Rideal–Eley mechanism at a certain temperature, and oxidized Ni catalyst is active for full oxidation of CH<sub>4</sub> [5,20]. The consumed reversibly adsorbed oxygen can be supplemented continuously by gas phase O2, which keeps the catalyst from being reduced (figure 12(a)). The oxidation of CH<sub>4</sub> by adsorbed oxygen is non-selective, and the products may be H<sub>2</sub>O and CO<sub>2</sub> or H<sub>2</sub>O, CO<sub>2</sub>, H<sub>2</sub> and CO depending on the temperature. High temperature is favorable for producing H<sub>2</sub> and CO, which is in agreement with the results published by Slagtern et al. [19].

The reaction between  $CH_4$  and adsorbed oxygen is not a fast one, which can be inferred by the consumption of  $CH_4$  and  $O_2$  (figure 10), otherwise, the conversions of  $CH_4$  and  $O_2$  will not be so low during the temperature-programmed reaction. With the increase of the temperature, the  $O_2$  adsorbing rate increases and is still faster than that of the reaction between  $CH_4$  and adsorbed oxygen, for  $CO_2$  and  $H_2O$  are always the main products, and  $O_2$  has not been used up. When the relative amount of adsorbed oxygen is not sufficient, CO and CO and CO and CO and CO and CO are produced.

After closing the  $O_2$  mass flow controller, the catalyst surface disengaged from  $O_2$  ambient undergoes an induction period and active metallic Ni sites are formed (figure 12(b)), so  $CH_4$  starts to decompose to  $H_2$  and  $Ni_xC$ , and  $Ni_xC$  reacts further with NiO to CO or  $CO_2$ .

When the  $O_2$  mass flow controller is re-opened, the catalyst is reduced due to the reaction between  $Ni_xC$  and NiO to CO or  $CO_2$ .  $CH_4$  competes with  $O_2$  to adsorb on active metallic Ni sites and decomposes immediately to  $H_2$  and  $Ni_xC$  (figure 12(c)).  $Ni_xC$  can react quickly with NiO from

Ni oxidized by  $O_2$  to CO or  $CO_2$  [13,14]. So the catalyst can maintain its reduced state. Furthermore, partial oxidation of  $CH_4$  proceeds via a direct oxidation route with the full consumption of  $O_2$ , therefore, the reaction rate,  $CH_4$  conversion, and the selectivities to  $H_2$  and CO can be improved significantly.

Thus, if the catalyst surface has been fully oxidized before letting the 2/1 CH<sub>4</sub>/O<sub>2</sub> flow into the reaction system, CH<sub>4</sub> can only undergo a non-selective oxidative reaction with adsorbed oxygen via the Rideal–Eley mechanism, which causes the rather low conversion of CH<sub>4</sub> and the selectivities to CO and H<sub>2</sub>. Only when the catalyst surface maintains its reduced state can CH<sub>4</sub> react with O<sub>2</sub> efficiently via a direct oxidation mechanism. Therefore, the surface state of the catalyst plays a crucial role in the conversion and selectivity of the reaction [20].

#### 5. Conclusions

At atmospheric pressure and 700 °C, if the catalyst surface is in its oxidative state, gas phase O2 will not be able to be used up and a certain amount of reversibly adsorbed oxygen will exist on the catalyst surface. Non-selective oxidation between CH<sub>4</sub> and reversibly adsorbed oxygen with high oxidation activity occurs easily via the Rideal-Elev mechanism, and both the conversion of reactants and the selectivities to H<sub>2</sub> and CO are very low. Thereby, during partial oxidation of CH<sub>4</sub>, the catalyst must be maintained in the reduced state. Thus, CH<sub>4</sub> can react with O<sub>2</sub> via a direct oxidation mechanism with high conversion and selectivity. O<sub>2</sub> being consumed fully, a small amount of carbon species on the catalyst surface during the reaction and CO disproportionation limited by thermodynamic equilibrium under such conditions [15] are the main reasons why the selectivity to CO is very high.

The results also indicate that direct oxidation is the main route for partial oxidation of CH<sub>4</sub>, and the indirect oxidation mechanism or combustion–reforming mechanism cannot gain dominance in the reaction under the experimental conditions.

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#### References

- A.M. Diskin, R.H. Cunningham and R.M. Ormerod, Catal. Today 46 (1998) 147.
- [2] S. Tang, J. Lin and K.L. Tan, Catal. Lett. 55 (1998) 83.
- [3] D.A. Hickman, E.A. Haupfear and L.D. Schmidt, Catal. Lett. 17 (1993) 223.
- [4] V.A. Tsipouriari, Z. Zhang and X.E. Verykios, J. Catal. 179 (1998) 283
- [5] D. Dissanayake, M.P. Rosynek, K.C.C. Kharas and J.H. Lunsford, J. Catal. 132 (1991) 117.
- [6] A.T. Ashcroft, A.K. Cheetham, J.S. Foord, M.L.H. Green, C.P. Grey, A.J. Murrell and P.D.F. Vernon, Nature 344 (1990) 319.
- [7] F.V. Looij, J.C.V. Giezen, E.R. Stobbe and J.W. Geus, Catal. Today 21 (1994) 495.
- [8] A. Guerrero-Ruiz, P. Ferreira-Aparicio, M.B. Bachiller-Baeza and I. Rodriguez-Ramos, Catal. Today 46 (1998) 99.
- [9] V.R. Choudhary, A.M. Rajput and B. Prabhakar, J. Catal. 139 (1993) 326
- [10] D.A. Hickman and L.D. Schmidt, Science 259 (1993) 243.
- [11] E.P.J. Mallens, J.H.B.J. Hoebink and G.B. Marin, J. Catal. 167 (1997) 43.
- [12] Y. Matsumura and J.B. Moffat, Catal. Lett. 24 (1994) 59.
- [13] S.K. Shen, C.Y. Li and C.C. Yu, Stud. Surf. Sci. Catal. 119 (1998)
- [14] S.K. Shen, C.Y. Li and C.C. Yu, Chin. J. Catal. 19 (1998) 309.
- [15] C.Y. Li, C.C. Yu and S.K. Shen, Chin. J. Catal. 19 (1998) 463.
- [16] T. Chen, W.Z. Li and C.Y. Yu, Chin. J. Catal. 19 (1998) 37.
- [17] R.A. van Santen and J.W. Niemantsverdriet, Chemical Kinetics and Catalysis (Plenum, New York, 1995) p. 75.
- [18] G.A. Somorjai, Introduction to Surface Chemistry and Catalysis (Wiley, New York, 1994) p. 50.
- [19] A. Slagtern, H.M. Swaan, U. Olsbye, I.M. Dahl and C. Mirodatos, Catal. Today 46 (1998) 107.
- [20] A.G. Steghuis, J.G. van Ommen and J.A. Lercher, Catal. Today 46 (1998) 91.